

The turbulence is a very important concept in wake modelling as it contributes the wake recovery while increasing the fatigue loads on the downstream turbine(s). It is taken into consideration in the wake model re-calibration process in terms of atmospheric turbulence intensity,  $TI = \frac{\sigma_U}{U}$ . It was computed using synchronous data extracted from the met-mast and the SCADA of the most upstream turbine in Lillgrund offshore wind farm during a winter and a summer day to see the seasonal effects.



The wind speed was calculated for each turbine iteratively using Horns Rev-I, Thanet and Lillgrund offshore wind farms and NREL 5 MW single turbine simulations [3]. Both cases have been investigated using second-wise datasets extracted during both normal operation and under curtailment.

#### NREL 5 MW

NREL 5 MW is an artificial turbine widely used in simulations since -contrary to commercial turbines- all the aerodynamic and geometric properties are published [3]. The scenario is 50 % downregulation with a simulated mean wind speed of 13 m/s.



Thanet dataset also includes curtailment which can be seen between 1.4 and 1.5 ·10<sup>5</sup>. The power curve is not representative after that point but the agreement between the effective wind speed and the nacelle wind speed proceeds with the same trend.

For Lillgrund, estimated effective wind speed is in a very good agreement with the synchronous met-mast data where nacelle anemometer measurements seem to include high level of noise.

### Horns Rev – DownRegulation

The second dataset from Horns Rev covers approximately 2 hours of data extracted during down-regulation. In Figure 2 (a), the characteristics of the downregulation which in total lasts approximately one hour may be seen.



Conclusion: the model is able to reproduce the wind speed averaged over the rotor for ; . Horns Rev - I (Vestas V80 - 2MW offshore), Thanet (Vestas V90 – 3MW offshore) and Lillgrund (Siemens SWT-2.3-93) offshore wind farms

- NREL 5 MW simulations
- Under both normally operated and downregulated cases.

#### **Conclusion:**

- 1. The effective wind speed (effWS) performs better than the nacelle wind speed (nws) when estimating the atmospheric turbulence intensity
- 2. effWS is in a good agreement with the met-mast data -> suitable to use in the wake model re-calibration

## Conclusion

Real-time wind farm scale available power estimation

Also to be used for real-time wind farm power curve

✓ Second-wise effective wind speed estimation using Active Power, Pitch and **Rotational Speed. Validated using:** 

- Horns Rev-I (optimum operated + down-regulated)
- Thanet (optimum operated + down-regulated)
- Lillgrund (optimum operated)
- NREL 5 MW (down-regulated)
- Effective wind speeds are used to estimate the atmospheric turbulence intensity and together they are used to calibrate GCLarsen single wake model for real-time
  - Significant improvement in wake recovery around ± 5° relative wind direction bin
- The calibrated model is then run on wind farm scale
  - Promising results were obtained applying time delay: maximum average error of 15.5%

# **Future Works**

- Re-parameterization of the wake algorithm considering meandering
  - Pragmatic approach using wind direction fluctuations [6]
- Real-time wake model implementation on other offshore wind farms Beginning with Horns Rev
- Uncertainty estimation of the available power estimation procedure in practice today and the developed algorithm
  - > Summation of individual available powers vs. algorithm described
- Validation of the final algorithm via wind farm scale experiments on Horns Rev
  - ✓ See Gregor Giebel's poster titled 'Experimental verification of a real-time power curve for down-regulated offshore wind power plants' PO.ID 087!

# Acknowledgements

The project partners of PossPOW are Vattenfall, Siemens, Vestas, and DONG. PossPOW is financed by Energinet.dk under the Public Service Obligation, ForskEL contract 2012-1-10763.

# **GCLarsen Wake Model Re-calibration for Real Time**

# **Re-calibrated Model Results – Single Wake**

#### The single wake model proposed by GCLarsen has been used for recalibration due to its robustness and simplicity. The model has been implemented in WindPro and shown to perform well also on offshore [4]. The GCLarsen velocity deficit for single wake is derived as below [5] with two variables that were modelled in terms of thrust coefficient, $c_T$ and atmospheric turbulence intensity, TI.

$$u_{x}(x,r) = -\frac{U_{\infty}}{9} (c_{T}A(x_{0} + \Delta x)^{-2})^{\frac{1}{3}} \left\{ r^{\frac{3}{2}} \left( 3c_{1}^{2}c_{T}A(x_{0} + \Delta x) \right)^{-\frac{1}{2}} - \left( \frac{35}{2\pi} \right)^{\frac{1}{10}} (3c_{1}^{2})^{-\frac{1}{2}} \right\}$$

With  $x_0 = a \cdot c_T^b$  and  $c_1 = c \cdot c_T^d + e \cdot TI$ . The estimated second-wise effective wind speed values in Thanet during normal operation were used for calibration and the model is validated on Horns Rev data. For recalibration of the wake model, all data was filtered for north-west perpendicular winds i.e. 320±30°. The model was fit to the dataset using nonlinear least squares estimates.



The original GCLarsen model significantly under-predicts the downstream wind speed for the second-wise dataset. Better recovery achieved by the recalibration can be observed even for 90°±5° bin.

## **Re-calibrated Model Results – Farm Scale**

70

Time it takes for a particle to move form the most upstream turbine(s) to the current turbine

**Upstream Distance** 

Average Percentage Error in Wind Speed

#### References

- 1.Heier, S., 1998, Grid Integration of Wind Energy Conversion Systems, John Wiley & Sons Ltd, Chichester, UK, and Kassel University, Germany
- 2.Raiambal, K. and Chellamuthu, C., 2002, "Modelling and Simulation of Grid Connected Wind Electric Generating System", Proc. IEEE TENCON, p.1847–1852
- 3.Jonkman, J., Butterfield, S., Musial, S. and Scott G., 2007, Definition of a 5-MW Reference Wind Turbine for Offshore System Development NREL/TP-500-38060 National Renewable Energy Laboratory, Golden, CO
- 4.Hansen, K. S., 2014, Benchmarking of Lillgrund offshore wind farm scale wake models. EERA DeepWind 2014 - 11th Deep Sea Offshore Wind R&D Conference, Trondheim, Norway, 22/01/14 5.Larsen G. C., 1998, A Simple Wake Calculation Procedure, Technical Report Risø-M-2760, Risø Roskilde, Denmark
- 6.Ainslie, J. F. (1986, March). Wake modelling and the prediction of turbulence properties. In Proceedings of the Eighth British Wind energy Association Conference, Cambridge, Mar (pp. 19-21).

Time Delay = **Average Wind Speed** 

- Upstream Distance is calculated using the most upstream turbine location and the averaged wind direction
- The effective wind speed at the most upstream location is averaged to approximate the time delay over 90mins

Conclusion: the recalibrated GCLarsen wake model is able to reproduce the downstream effective wind speed for single wake case. On farm scale, time delay is critical for validation cases and the model can be further enhanced by a dynamic time delay algorithm as well as practically introduced meandering. The finalized algorithm can easily be used to achieve realtime wind farm power curve under various operational conditions.





EWEA Offshore 2015 – Copenhagen – 10-12 March 2015

