

# New lubrication device to minimize wear at the pitch gear

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## Abstract

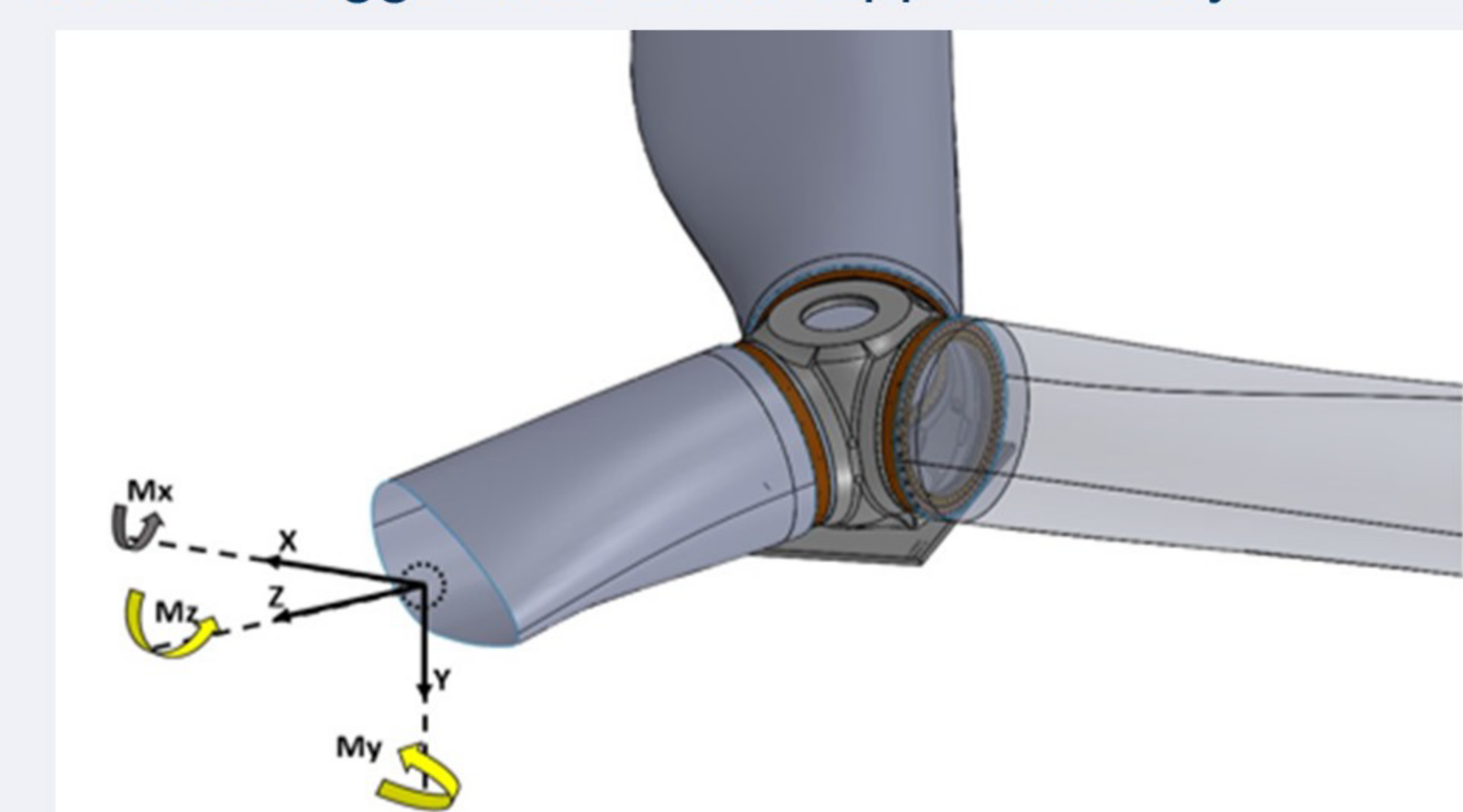
At low wind speeds the pitch system works at the 0° position without movement. When the wind turbine approaches its nominal power, the pitch system starts to actuate inducing oscillations into the system due to the **continuous movement of the pitch** due to the thrust and the wind speed changes. The dynamic operation during long periods in the same position **reduces the lubricant thickness** between the teeth and consequently causes direct contact between the two metal surfaces. This factor together with the lower crown surface hardness causes **excessive wear** as defined ANSI/AGMA 1010-E95 in the zero position as reports Holierhoek [1].

Patented solutions to minimize the gear wear at specific points like the 0° pitch position exist. The proposed solutions essentially tune parameters such as surface state [2-3], stress, mechanical contact [4] and tribology [5-7]. However, the solutions presented in [2-3] cannot eliminate the preventive maintenance, while the solutions in [4-5] require expensive parts such as another pinion and a compressor. The solution in [6] **requires programed stops of the turbine which cause generation losses**, and the solution in [7] is difficult to integrate in ongoing wind turbines due to the necessity of pinion replacement.

In spite of these issues, the most used solution is the lubrication pinion presented in [6], therefore the new lubrication device called **MiCRoLuBGear** is a complement that can avoid the lubrication programed stops and consequently **increase the electricity generation and reduce wear**.

## Objectives

To manufacture the **new MiCRoLuBGear** devices micro-fabrication technology is used. The main challenge in these dimensions is the control of the grease flow dynamics in dimensions smaller than 1 mm, which has not been previously studied. Our previous studies [8] showed that the device has an appropriate performance for gear modules up to 12, commonly used at wind turbines of 2 MW. The dedendum free space increases as the gear module increases, so the device will be useful for wind turbines bigger than 2 MW approximately.



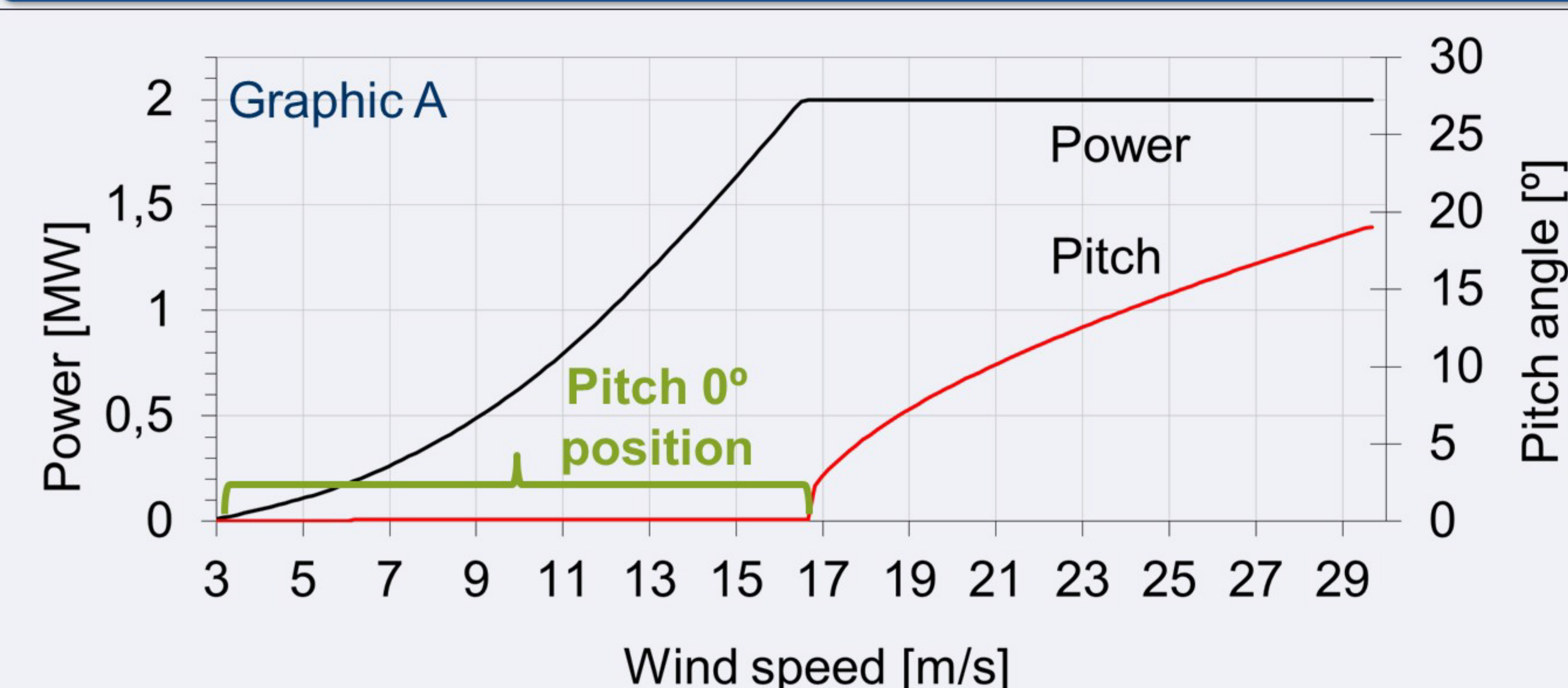
Therefore, to validate **MiCRoLuBGear** device Micro Particle Image Velocimetry ( $\mu$ PIV) is used to analyze the flow behavior of a NLGI grade 1 and 2 greases in channels that can be integrated in a 12-module gear. Samples of the injected grease were collected to verify that grease had not degraded during flow in the micro-channel. Furthermore the influence of the temperature on the device behavior is validated at temperatures from -20°C using greases NLGI grade 1 and 2, useful for wind turbines that operate under cold climate conditions.

The  $\mu$ PIV results and the cold climate operation behavior are used to define the integration of the lubrication device in the wind turbine lubrication circuit and to define a lubrication strategy to inject fresh grease at the pitch zero degree position.

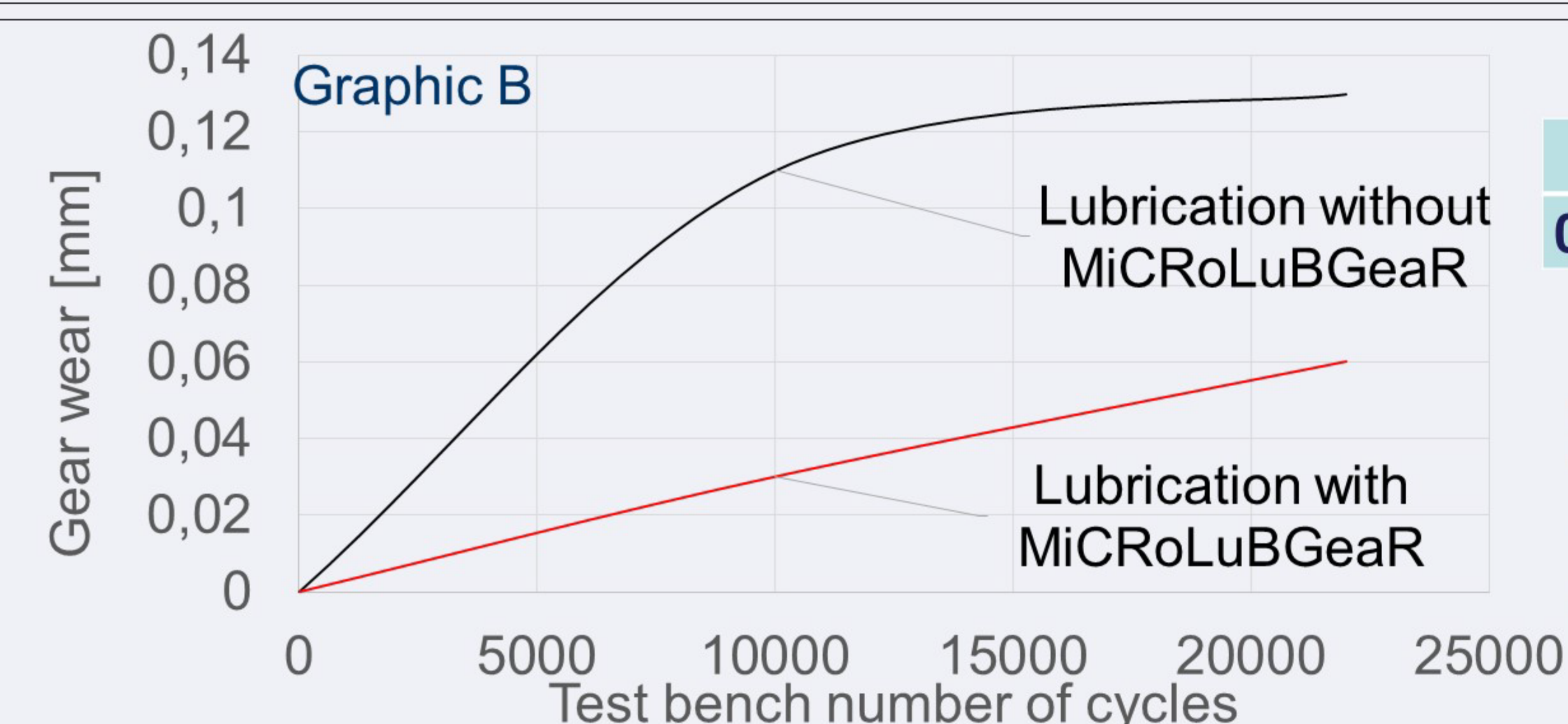
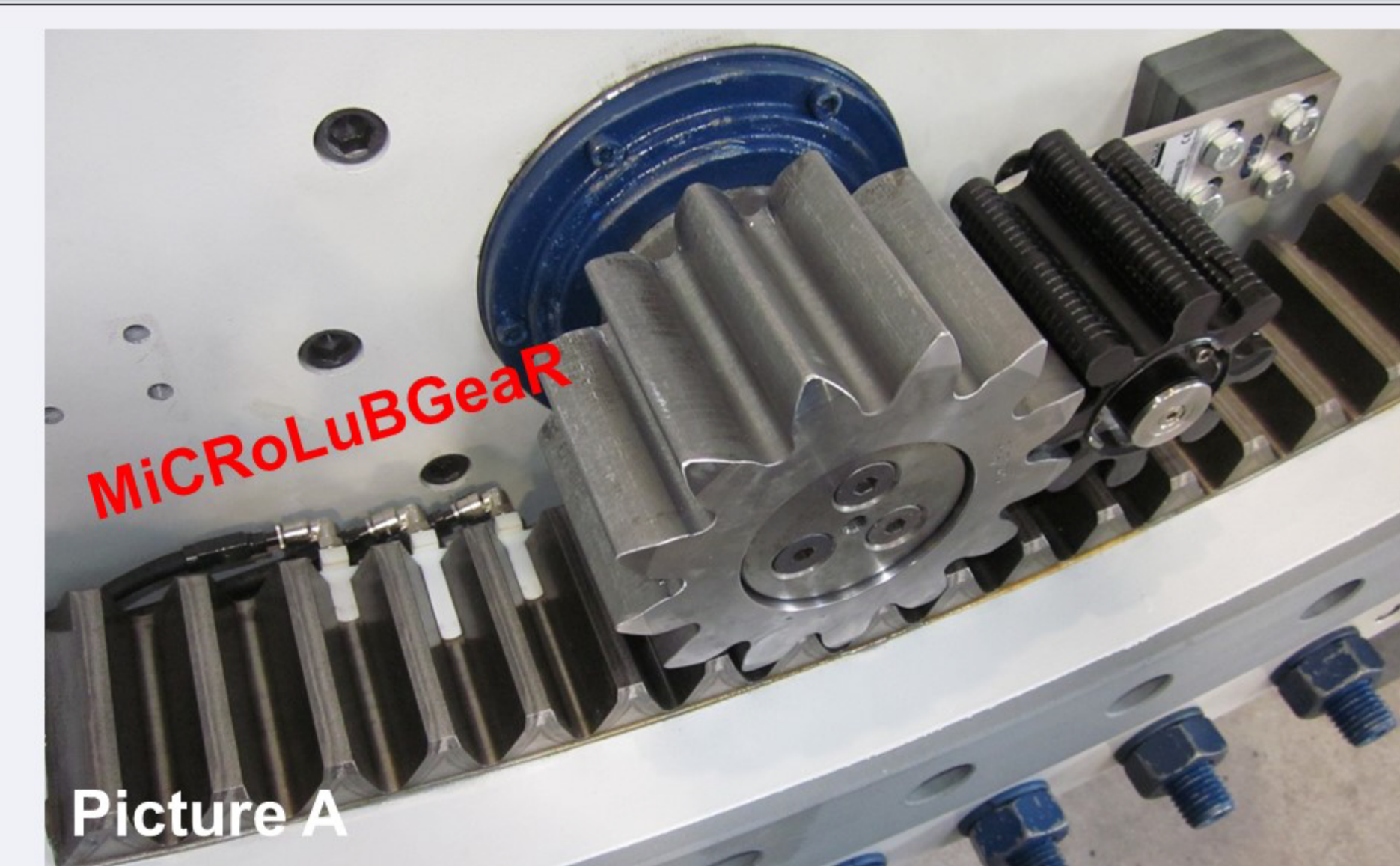
A novel test bench is built to reproduce the phenomena of the excessive wear at the 0° position of the pitch. The main factors needed to reproduce the excessive wear due to the wind turbine dynamic operation in the test bench are:

- The blade micro movements caused by the gearbox backlash and the torque caused by the aerodynamic forces of the blade to turn around its axis. To simulate this, a constant torque  $M_z$  [9] is preassembled to the blade and a 0.034° oscillation (0.5 mm of backlash in the crown of M12 and Z139) is applied through an electric motor.
- The stress cycle traction and the compression on the blade when the pitch works in the 0° position. This is simulated in the test bench by  $M_x$  and  $M_y$  at 0.3 Hz to simulate the blade revolution in operation.

## Methods



The graphic A shows the pitch operation at zero degree position for low velocities where the wind turbine operates an average of 60% of the time. For this reason it is required programmed stops to lubricate the teeth. The picture A shows MiCRoLuBGear installed to lubricate the tooth under operation to avoid programed stops and consequently increase energy generation.



### TEST BENCH LOADS

Backlash	$M_z / M_{\text{torsion}}$	$M_x / M_{\text{edge}}$ and $M_y / M_{\text{flap}}$
0.5mm at 0.2Hz	Constant $\pm 40$ KNm	2000 kNm at 0.3Hz

A test bench validation of 2MW pitch bearing was performed with the loads defined in the previous table. To quantify the evolution of the teeth wear, teeth molds was obtained at different test bench cycles as picture B shows. The wear evolution it is represented in the graphic B showing a lineal wear evolution until the wear starts at the adjacent tooth and consequently it is reduced. The wear using MiCRoLuBGear it is reduced more than 70%.



## Conclusions

This study demonstrates **MiCRoLuBGear** can properly lubricate pitch teeth at zero degree position and **reduce gear wear up to 70%** respect to current technologies while the wind turbine operates. The technology is **easy to implement in all ongoing** wind turbines and the current automatic lubrication systems. Additionally MiCRoLuBGear can operate **in environments of cold condition until -20°C**. These characteristics improve the low efficiency of current lubrication systems that generates energy generation losses. Furthermore, these losses will increase in future wind turbines; this novel technology is a key element in the contribution to make the new multi megawatt **wind turbines more profitable**. The technology presented also becomes essential in offshore wind turbines where the maintenance reduction is of high importance.

## References

1. J.G. Holierhoek, H. Korterink, R.P. van de Pieterman, H. Braam, L.W.M.M. Rademakers, D.J. Lekou, T. Hecquet, H. Söker; September 2010. Recommended Practices for Measuring in Situ the 'Loads' on Drive Train, Pitch System and Yaw System. Protest ECN-E--10-083.
2. Mashue A, Moorer B.G, Goodwin K, inventors; 2011 Jun. 16. Gear set for pitching blade of rotor of wind turbine utilized for providing electricity to utility grid, has pinion/drive gear comprising set of teeth whose hardness is less than harness of teeth of ring gear. United States patent US 2011142617-A1.
3. Dimascio P, Close R, Auer G, Grimley R, Hamel A, inventors; 2009 Aug. 29. Hub pitch gear repair method. Canada patent CA 2655691-A1.
4. Nielsen T, inventor; 2008 Jun. 26. A gear system for yaw drive or a pitch drive for a wind turbine. World Intellectual Property Organization WO 2008/074320-A1.
5. Kürzdörfer, M inventor; 2007 Mar. 21. Anstellwinkleinstellvorrichtung für eine Windkraftanlage. European Patent EP 1764544-A2.
6. Zdravko Paluncic, Andreas Schöenfeld inventors; April 26 2007. Lubricating device with lubricating pinion. European Patent DE202006011330-U1
7. Klaus P, inventor; 2010 Apr 20. Actuator for adjusting a rotor blade pitch angle. United States patent US 7699584-B2.
8. Lars G. Westerberg, Josep Farré-Lladós, Jinxia Li, Erik Höglund, Jasmina Casals-Terré; 30 January 2015. Grease flow in an elbow channel. Tribol. Lett. DOI 10.1007/s11249-015-0469-6
9. Germanischer Lloyd Industrial Services GmbH; July 2010. Guideline for the Certification of Wind Turbines. Germanischer Lloyd, Hamburg.

